Piezoelectric Filters with an Inductor having a Given Coupling

Card 2/3

frequencies in the arms of the filter are such that there is one frequency in the stop-band at which voltageresonance (for low-pass filter) or current-resonance (for high-pass filter) occurs. The characteristic attenuation has three poles (frequencies of infinite attenuation). The dynamic attenuation has an extra pole at a frequency when the impedances of all the filter arms become simultaneously zero or infinite. Formulae for calculation of the values of the elements of both balanced and unbalanced filters, Eqs (1) - (6), were taken from Velikin et al. (Refs 2,3). In the formulae: RHOm - is the meminal impedance of the filter, - is the resonant frequency of the resonators. The initial data is the boundary frequency fa and the attenuation poles for, for, for and fu. In filters, attenuation poles f_{∞} , f_{∞} , f_{∞} and f_{μ} . In filters, with the circuits given in Fig 4a and 5a the calculated value of the coupling coefficient of the inductor windings is of the order of 10%. The construction of the coil is shown in Fig 8. The desired value of the

SOV/106-58-12-8/13

Piezoelectric Filters with an Inductor having a Given Coupling Coefficient

coupling coefficient is obtained by spacers, and the Q-factor depends on the core material. The author then investigates the temperature dependence of the coupling coefficient.

There are 9 figures and 8 references, 5 of which are Soviet, 2 English and 1 German.

SUBMITTED: December 25, 1957

Card 3/3

GEL'MONT, Z. Ya., Candidate Tech Sci (diss) -- "Investigation of piezoelectric filters for lower and higher frequencies". Leningrad, 1959. 12 pp (Min Communications UNSR, Leningrad Electrical Engineering Inst im Prof M. A. Bonch-Bruyevich), 150 copies (KL, No 23, 1959, 165)

8982.9 s/105/60/000/011/004/010 1055/1033 Velikin, Ya.I., Gelimont, Z.Ya., and Zelyakh, E.V. A Piezoelectric Band-Elimination Filter Circuit. 9,7550 AUTHORS: The band-elimination quartz filters have usually a comparative-PERIODICAL: Filektrosvysz', 1960, No.11, pp. 34-39 ly low impedance in the region of the suppressed frequencies.

1y low impedance in the region of the suppressed frequencies. ly low impedance in the region of the suppressed frequencies. In some have practical cases, it is sometimes necessary, however, for the filter circuits, bractical cases, it is sometimes necessary, however, for the filter circuits, it is sometimes necessary, however, for the filter circuits, bractical cases, it is sometimes necessary, however, for the filter to have practical cases, it is sometimes necessary, however, for the filter to have practical cases, it is sometimes necessary, however, for the filter to have practical cases, it is sometimes necessary, however, for the filter to have practical cases, it is sometimes necessary, however, for the filter to have practical cases, it is sometimes necessary, however, for the filter to have practical cases, it is sometimes necessary, however, for the filter circuits, and the considerable impedance in the suppressed band. Two such filter circuits, and the considerable impedance in the suppressed band. TITLE: a considerable impedance in the suppressed band. Two such filter circuits, lace on the suppressed band. Two such filter circuits is a containing one and two piezoelectric resonators respectively (see Fig. 1a containing one and two piezoelectric resonators frequency of the filter circuits have containing one and two piezoelectric resonators frequency of the resonator (shunted by a containing one and two piezoelectric resonators one and a narrow one. The resonator (shunted by a really two suppression bands: a wide one and a narrow one. really two suppression bands: a wide one and a narrow one. The narrow by a in the region of the antiresonance frequency of the resonator (shunted by a capacitance) is the principal one and is used for the compression of capacitance), is the principal one and is used for the suppression of 1 capacitance), is the principal one and is used for the suppression of currents of given frequencies. Its width is somewhat larger in the circuit currents of given frequencies. 8. currents of given frequencies. Its whath is somewhat larger in the circuit containing two resonators. Using equivalent circuits for his dischasion, and the substantial than the substantial than the substantial transfer the effective ettennation in the substantial transfer the effective ettennation in the substantial transfer the effective ettennation in the substantial transfer transfer the effective ettennation in the substantial transfer containing two resonators. Using equivalent circuits for his discussion, the suppression and the suppression and the suppression and the filter direct containing two resonators. рi the Euthor calculates the ellective attenuation in the suppression . The suppression of the filter circuit conestablishes first a general formula for the case of the filter circuit conestablishes first a general formula for the case of the filter circuit conestablishes first a general formula for the case of the filter circuit conestablishes first a general formula for the case of the filter circuit conestablishes first a general formula for the case of the filter circuit conestablishes first a general formula for the case of the filter circuit conestablishes first a general formula for the case of the filter circuit conestablishes first a general formula for the case of the filter circuit conestablishes first a general formula for the case of the filter circuit conestablishes first a general formula for the case of the filter circuit conestablishes first a general formula for the case of the filter circuit conestablishes first a general formula for the case of the filter circuit conestablishes first a general formula for the case of the filter circuit conestablishes first a general formula for the case of the filter circuit conestablishes first a general formula for the case of the filter circuit conestablishes first a general formula for the case of the filter circuit conestablishes for the case of the ca an. SUB. card 1/2W Card 2 CIA-RDP86-00513R0005147100

9.2186 (1063,1159)
9.3230 (1132,1040)

3587 S/108/61/016/011/003/007 D201/D304

AUTHORS:

Velikin, Ya.I., Gel'mont, Z.Ya., and Zewakh E.V., Members of the Saciety

TITLE:

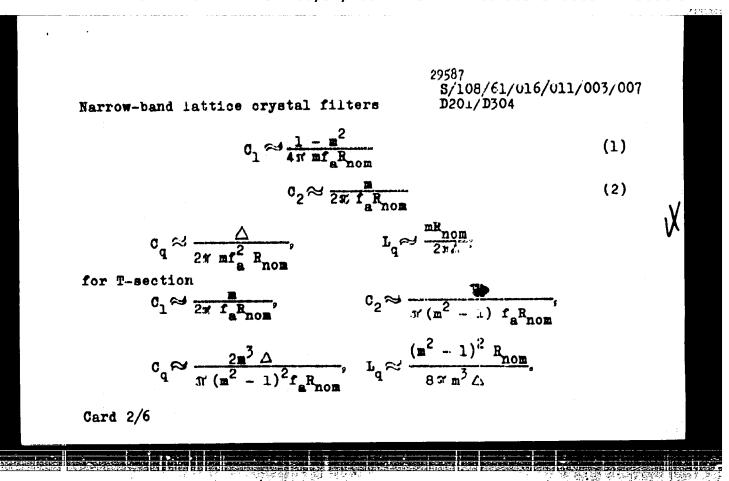
Narrow-band lattice crystal filters

PERIODICAL: Radiotekhnika, v. , no. 11, 1961, 26 - 33

TEXT: In the present article design formulae are derived for lattice filters consisting of a piezoelectric crystal and a capacitor and forming a single, two-, three and four-section networks. The analysis of the filters is made using basic W- and T-sections, as shown in Figs. la and 2a. Although design formulae for the above configuration are given in literature, for narrow pass-band filts smaller than e.g. 0.05, simpler approximate formulae may be used 6: Metod rascheta ekvivalentnykh skhem (Method of Designing Equivators Circuits Nauchno-tekhn. sb. po elektrosvyazi Leningr. in-ta svyazi no. 6, 1946). These formulae are as follows: for N-section Card 1/6

"APPROVED FOR RELEASE: 08/31/2001

CIA-RDP86-00513R000514710008-5



Narrow-band lattice crystal filters D2

29587 S/10e/61/016/011/003/007 D201/D304

For both cases

$$\mathbf{m} = \sqrt{\frac{f_2^2 - f_{\infty}^2}{f_1^2 - f_{\infty}^2}} \tag{3}$$

and

$$\Delta = f_2 - f_1, f_a = \frac{1}{2} (f_1 + f_2)$$
 (4)

where f_1 and f_2 out-off frequencies, f_∞ - frequences of the attenuation band, R_{nom} - characteristic filter impedance at frequency f_a . For narrow-band filters, as frequencies near f_e .

$$\mathbf{m} \approx \sqrt{\frac{\mathbf{f}_2 - \mathbf{f}_{\infty}}{\mathbf{f}_1 - \mathbf{f}_{\infty}}} \tag{5}$$

may be assumed and hince, introducing

(6)

$$\Delta_{\infty} = 2(\mathbf{f}_{\infty} - \mathbf{f}_{\mathbf{a}}), \quad \mathbf{t} = \frac{\Delta_{\infty}}{\Delta} \tag{6}$$

Card 3/6

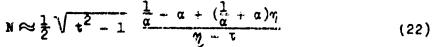
29587 S/108/61/016/011/003/007 D201/D304

Narrow-band lattice crystal filters

the approximate expression for m is obtained as

$$\mathbf{z} \approx \sqrt{\frac{t-1}{t+1}} \,, \tag{7}$$

which is the generalized equation (does not contain frequency). The attenuation of the single section filter is derived as



where $\alpha = \frac{R_o}{R_{nom}}$, and η given by

$$\eta = \frac{f - f_a}{\frac{1}{2}\Delta} \tag{19}$$

- the normalized frequency (Ref. 6: Op. cit.). For the two-section filter the anntenuation is derived as

Card 4/6

Narrow-band lattice crystal filters

29587 \$/108/61/016/011/005/007 D201/D504

$$N \approx \sqrt{t^2 - 1} \frac{\left[\frac{1}{\alpha} - \alpha + \left(\frac{1}{\alpha} + \alpha\right)\eta\right](\eta t - 1)}{\left(\eta - t\right)^2},$$
 (27)

for three-section
$$N \approx \frac{1}{2} \sqrt{t^2 - 1} \left[\frac{1}{\alpha} - \alpha + (\frac{1}{\alpha} + \alpha) \gamma \right] \frac{4(\eta t - 1)^2 - (t - \eta)^2}{(t - \eta)^3}$$
and four-section as

and four-section as

$$N \approx 2\sqrt{t^2 - 1} \left[\frac{1}{\alpha} - \alpha + (\alpha + \frac{1}{\alpha}) \eta \right] (nt - 1) \frac{2(\eta t - 1)^2 - (\eta - t)^2}{(\eta - t)^4};$$

Each of tehm simplifies according to the values of load and the respective values of η and to the values of load and the respective values of η and to the above filter circuits may, in particular be used for crystal filters at frequencies above 1 mc/s, with transverse oscillating crystals of AT and BT cut. Experimental two- and three- Π -section filters operating at the center pass-band frequency of 1364 kc/s had a pass band of 800 c/s. There are 8 figures and 7 references: 4 Soviet-bloc and 3 non-Soviet-bloc. The Card 5/6

²⁹⁵⁸⁷ s/108/61/016/011/003/007

Narrow-band lattice crystal filters

reference to the English-language publication reads as follows: R. A. Sykes, IRE National Convention; part 2, 1958.

ASSUCIATION:

Nauchno-tekhnicheskoye obshchestvo radiotekhniki i elektrosvyazi im. A.S. Popova (Scientific and Technical Communication im. A.S. Popov) [Abstractor's note: \ Name of Association taken from 1st page of journal]

SUBMITTED:

April 29, 1960 (initially)
July 7, 1961 (after revision)

Fig. 1.

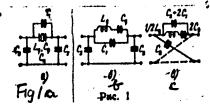
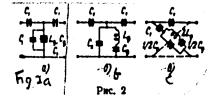


Fig. 2.



Card 6/6

CIA-RDP86-00513R000514710008-5" APPROVED FOR RELEASE: 08/31/2001

BOROVINSKAYA, D.A.; GEL'MONT, Z.Ya.

Upper frequencies quarts filter using an overlapped T-network.
Elektrosvias' 17 no.5:34-40 My '63. (MIRA 16:4)

(Electric filters) (Radio filters)

\$/065/60/000/006/006/006/XX E194/E484

AUTHORS: Agafonov, A.V., Gel'ms, I.E. and Rabikovich, E.I.

TITLE: The Selection of Catalyst for Cracking Residual

Petroleum Fractions and Study of its Poisoning During

the Process

PERIODICAL: Khimiya i tekhnologiya topliv i masel, 1960, No.6,

pp.6-12

TEXT: A special feature of the operating conditions of catalyst when cracking residual feed is the high rate of poisoning of the catalyst by the combined influence of temperature, steam, sulphur compounds and resinous substances containing metallo-organic compounds. The poisoning is specially marked with catalyst in powder form. The high molecular hydro-carbons of the heavy part of the feed are the main source of products that are of low stability at temperatures used for cracking so that there is no need for a great reduction in the energy of activation. Moreover, the use for this purpose of high activity catalysts is accompanied by considerable increase in gas and coke formation. The measure of the necessary activity of catalyst used in cracking residual feed should be the production of gasoline of good engine properties combined with Card 1/4

s/065/60/000/006/006/008/xx E194/E484

The Selection of Catalyst for Cracking Residual Petroleum Fractions and Study of its Poisoning During the Process

favourable gas composition and a high rate of conversion of the residual fractions. It is desirable to use large plants for cracking residual fractions which requires large quantities of catalyst of appropriate quality. It is found that the requisite conditions are satisfied by fire-resistant high-alumina kaolin clays, many kinds of which after simple heat treatment have sufficiently good and stable catalytic properties. Table 1 gives the characteristics of semi-industrial quantities of natural catalysts obtained from various natural clays. In this table the activity of the catalysts is characterized by the cracking of light feed as this gives the more sensitive index of performance. is then considered and Table 2 gives experimental data about the Catalyst poisoning deactivation of a simple, natural, microspherical catalyst. Characteristics of the cracker feed-stocks are given in Table 3. The tests, results of which are given in Table 2, were continued for 20 days and the observed changes in catalyst properties may be considered as the results of poisoning by metals and sulphur combined with poisoning due to reduction in the surface and porosity

S/065/60/000/006/006/008/XX E194/E484

The Selection of Catalyst for Cracking Residual Petroleum Fractions and Study of its Poisoning During the Process

caused by heat and steam. The selectivity of the catalyst was much reduced. Comparison between the test results and those of laboratory tests with artificial poisoning of the catalyst by metal showed that in the tests most of the poisoning was due to metals and not sulphur, see Table 4. The influence of metals deposited on the catalysts on certain characteristics of cracking of distillate and crude oil feeds are given in Table 5. Note should be made of the much smaller degree of poisoning of the catalyst by an equal quantity of deposited metal when cracking residual feed rather than distillate. The influence of steam was studied in the laboratory and the results are given in Table 6; it will be seen that treatment of poisoned catalyst by steam promotes recovery of activity and improves the selectiveness. It is concluded from the work that catalytic cracking of residual feed stock on microspherical natural catalyst is practical and a stable process can be The capital cost of constructing a catalyst manufacturing works should not be above 500 roubles per ton of catalyst produced per year. Investment in quarries and other Card 3/4

\$/065/60/000/006/006/008/xx E194/E484

The Selection of Catalyst for Cracking Residual Petroleum Fractions and Study of its Poisoning During the Process

workings is from 100 to 200 roubles per ton per year. The cost of one ton of finished catalyst is about 400 roubles. calculated that the use of natural catalyst rather than synthetic economizes both capital investment in the production of catalyst and the cost of the first charge by not less than 15 roubles for each ton per year of feed stock delivered for catalytic crackings. Accordingly, the economy that results from the use of natural rather than synthetic catalyst for cracking residual feed stock is considerable. There are 6 tables and 8 references: 2 Soviet and 6 English.

ASSOCIATION: VNII NP

Card 4/4

CIA-RDP86-00513R000514710008-5" APPROVED FOR RELEASE: 08/31/2001

SKURKO, Roman Isayevich; POCHERNIKOVA, Kaleriys Andreyevna;

GEL'MS, I.E., red.; KLEYMENOVA, K.F., ved. red.; VOHONOVA,

V.V., tekhn. red.

[Production of synthetic catalysts for petroleum refining]

Proizvodstvo sinteticheskikh katalizatorov dlia neftepererabotki.

Pod red. i s dop. I.E.Gel'msa. Hoskva, Gostoptekhizdat, 1963.

117 p. (MIRA 16:5)

(Catalysts) (Petroleum--Refining)

APPROVED FOR RELEASE: 08/31/2001 CIA-RDP86-00513R000514710008-5"

DAVYDOV, B.N.; BASOV, A.U., GELES, I.E.

Cost of spent well street and inflored in the shim. no.5:17-20
(MIRA 17:8)

1. Vacebynanyy manches-inflored tell liv in titut po pererabotke nefti i gaza i polucieniya labunatvencege zhickego topliva.

GEL'MS, I.E.; DAVYDOV, B.N.

Problems of economics in the development of the production of catalysts for the petroleum industry. Khim. i tekh. topl. i masel 9 no.3145-48 Mr*64 (MIRA 17:7)

1. Vsesoyuznyy nauchno-issledovateliskiy institut po pererabotke nefti i gazov i polucheniyu iskusstvennogo zhidkogo topliva.

Coping with the rated capacity of mine No.8 of the "Prokop'yevskugol'"Trust. Ugol' 38 no.11:8-10 N '63.

(MIRA 17:9)

1. Gornyy fakul'tet Sibirskigo metallurgicheskogo instituta

1. Gornyy fakul'tet Sibirskigo metallurgicheskogo instituta (for Gubin). 2. Glavnyy inzh. shakhty No.8 tresta Prokop'-yevskugol' (for Mogilevskiy). 3. Shakhta No.8 tresta Prokop'yevskugol' (for Gel'mut).

APPROVED FOR RELEASE: 08/31/2001 CIA-RDP86-00513R000514710008-5"

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GINIAL J.: COTTAIL, N.

"Flying in Cobaj-type Gilders ever the Peskids", N. 526, (CRIMA WACTI, Vol. 2, No. 22, Cotober 1953, Fraia, Czech.)

CC: Fonthly List of East European Accessions (FEAL), No. 10, Vol. 4, No. 3, March 1955, Uncl.
```

GEINAP, J.; PEK, L.

Gelnar, J.; Rek, L. Over the undulating Peskids. p.375. Fight against fear; a discussion. (Conclusion) p.377.

No. 16, Aug. 1955 KPIPIA VIASTI Praha, Czechoslovakia

SO: Monthly List of East European Accessions, (EFAL), IC, Vol. 5, No. 4 February, 1956

一十月四年五十十十月

GELLIAN.

GEOGRAPHY & GEOLOGY

CESKY LID.

Periodicals: APTEROPOZOINUM. Vol. 45, No. 5, 1958.

GEINAR, J. Rhytimic classification of our sengs of the eastern (vecal) type. p. 207.

Monthly List of East European Accessions (FEAI) LC Vol. 8, No. 4, April 1959. Unclass.

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JEDRZEJEWSKI, Włodzimierz; CELO, Helena

Application of amperometry in kinetic methods of quantitative analysis. II. Catalytic determination of microgram amounts of chromium (IV). Chem anal 7 no.4:753-758 162.

1. Katedra Chemii Nicorganicznej, Uniwersytet, Lodz.

ŒLO, J.

Potentiometric Determination of Na2S in the Waste Sulfite Liquor, p. 102.

PRZEGIAD PAPIERNICZY (Ministerstwo Przemyslu Drzewnego i Papierniczego oraz Stowarzyszenie Naukowe-Techniczne Inzynierow i Technikow Przemyslu Papierniczego)
Lodz, Poland
Vol. 11, no. 1, April 1958.

Monthly List of East European Accessions Index (EFAI), LC, Vol. 8, No. 11, November 1959. Uncl.

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P. Hardi

POLAND / Chemical Technology. Chemical Products and Hamber Application. Cellulose and Its Derivatives. Paper.

Abs Jour: Ref Zhur-Khimiya, No 9, 1959, 33539.

Author : Gelo, J. Wasiak, B.

Inst : Not given.

Title : Determination of Na₂S, NaOH and Na₂CO₃ with An

Alkali Sulfate.

Orig Pub: Przegl. papiern., 1958, 14, No 9, 255-268.

Abstract: By a proposed method, Na2S is determined iodo-

metrically after a preliminary precipitation of the organic substances by an acueous alcohol solution of BaCl₂. NaOH and Na₂CO₃ are determined by titration with 0.5 n. HCl after the preliminary removal of the sulfide by 0.1 n. ZnSO₄

Card 1/2

287

APPROVED FOR RELEASE: 08/31/2001 CIA-RDP86-00513R000514710008-5"

POLAND / Chemical Technology. Chemical Products and Their Application. Cellulose and Its Derivatives. Paper:

Abs Jour: Ref Zhur-Khimiya, No 9, 1959, 33539.

Abstract: solution. The method is verified in a number of processed alkali and in white alkali. Due to the simplicity and speed of the analysis, this method insures satisfactory accuracy in industrial supervision. -- From the authors' summary.

GELO, Jan, mgr

Comparison of two methods of determining the floating and swelling capacity of rayon grade pulps during the steeping process. Przegl papier 21 no.1:1-5 Ja 165.

1. Pulp and Paper Institute, Lodz. Submitted October 1964.

S/169/62/000/009/058/120 D228/D307

AUTHORS:

Grammakov, A. G., Gelobovskaya, V. S. and Khaykovich,

I. M.

TITLE:

Some problems of the theory of the helium method

PERTODICAL:

Referativnyy zhurnal, Geofizika, no. 9, 1962, 42-43, abstract 9A281 (In collection: Vopr. rudn. geofiz.,

no. 3, M., Gosgeoltekhizdat, 1961, 3-21)

TEXT: The basic theoretical principles of the helium method of seeking uranium deposits are given. The method is based on the fact that much of the He⁴ is a radioactive decay product of elements of the uranium and thorium series. Part of the helium escapes in consequence of the crystal lattice being disturbed. The migration of escaping helium is considered on the basis of the diffusion theory; this allows use to be made of the developed theory of gas surveying and takes into account that helium is formed continuously in rocks through which it diffuses. The following points are considered: the stationary distribution of gas in rock; and the

Card 1/2

Some problems of...

S/169/62/000/009/058/120 D228/D307

possible helium concentration over uranium orebodies, in the form of endless beds with a uniformly distributed concentration, and over globularly and cylindrically shaped bodies. The question of establishing the stationary state and of estimated a deposit's age is studied. The results of calculating the distribution of helium on models and contrivances are given; they can be used to determine the coefficients of diffusion of gases under field and laboratory conditions. It is concluded that the helium method can be expediently used in areas where rocks have low diffusion factors (~10⁻⁵ cm/sec²). The question is raised about the creation of accurate and highly sensitive equipment and about the method's further development. / Abstracter's note: Complete translation. /

Card 2/2

BENCZE, Bela, dr. GELOCZY, Ferenc, dr.; TOTH, Maria, dr.; UGRAI Mil:losne, dr.

Quantitative changes in the tocopherol (Vitamin E) content of the blood serum in the course of life. Gyermekgyogyaszat 15 no.6:176-183 Je¹64

1. A Bidapesti Orvostudomanyi Egyetem I. sz. Gyermekklinikajanak (Igazgato: Gegesi Kiss, Pal, dr. akademikus, egyetemi tanar) kozlemenye.

USSR/Diseases of Farm Animals - Diseases Caused by Helminths. R.

Abs Jour : Ref Zhur - Biol., No 6, 1950, 26336

Author : Gelovani, D.I.

Inst : Thilisi Zoological and Technical Institute of Veterinary

Sciences.

Title : General Influence of Stannum Arsenate on Chickens and

Its Toxicity.

Orig Pub : Materialy 12-y Nauchn. konferentisii, posvyashch.

25-lyetiyu Gruz. zootekhn.-vet. in-ta Tbilisi, 1957, 32-

36.

Abstract : The anthelmintic effectiveness stannum arsenate (I) was

tested on chickens infestated by cystoliths or ascaridae, as well as on chickens with mixed infestations.

(I) was administered to the chickens internally after

10 to 20 hours of fasting in the form of gelatin

Card 1/2

USSR/Diseases of Farm Animals - Diseases Caused by Helminths.

2.

Abs Jour

: Ref Zhur - Diol., No 6, 1950, 26336

capsules in dosages of 0.1, 0.12 and 0.15 grams per each adult chicken (after four hours the chickens were fed). The most effective (one hundred percent extensive and intensive effectiveness) dosage was found to be 0.15 grams. The toxic dosage of (I) is eight times larger than the therapeutic dosage, and therefore (I) may be used in group administrations to chickens. Young chickens are more sensitive to (I).

Card 2/2

26

CIA-RDP86-00513R000514710008-5 "APPROVED FOR RELEASE: 08/31/2001

Combry

: Farm Animals. General Protlems. CATEGORY

ABS. JOUR. | RZB101., No. 4, 1959, No. 16602

AUTHOR

INST. TITLE : Gelovani, D. N.:
: Georgia Zootechnical-Veterinary Institute.
: The Application of Antibiotics in Animal

Kusbandry.

ORIG. PUB. : Y sb.: Laterialy 13-y Maucha. To Merentali

(Gruz. zootekhn.-vet. in-t). Ch. 2, Thillist,

ABSTRACT : No abstract.

CARD:

1/1 *1957**,** 12-15

GEAUTARE, D. III

APPROVED FOR RELEASE; 08/31/2001 100 CIA-ROPS6: 00513R000514710008-5"

Agents
ABS. JOUR. : FZhPiol., No. 5 1259, No. 23202

AUTHOR

INST.

: Gelovani, D. M. : Georgian Zootechnical Veterinary Institute

: On Some Pharmacological Properties of the Alka-TITLE

loid Salsolidin

ORIG. FUB.

: Shrometa krebull. Sakartvelos zootekimikur-save-

ABSTRACT

terinaro instituti, Sb. tr. Gruz. zoctekim.-vet. DL100 of salsolidin (I) for mice in subcutaneous introduction is 10 mg, and the minimal telerated dose is 5 mg. The dopressor influence of I and salsolin (II) upon blood pressure depends on direct depressive action upon vasomotor centers and, to a lesser degree, on their direct vasodilative

*in-t, 1956, 1957 (1958), 9, 135-143

Card:

1/2

GELOVANI, M. A.

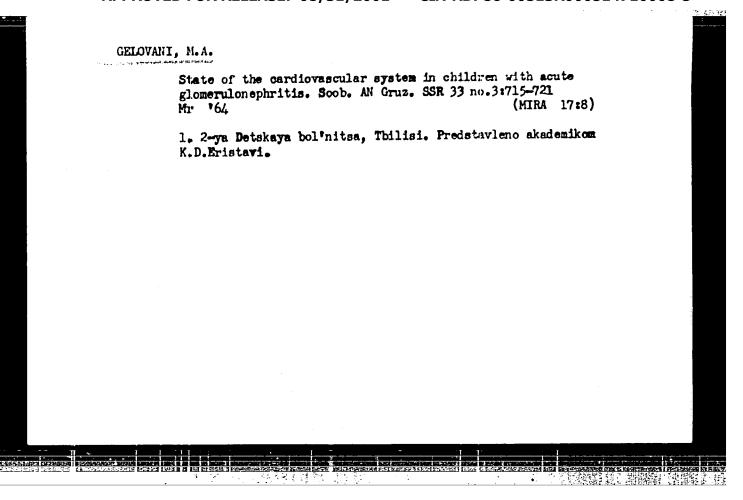
"Data on the Study of the Secretory Function of the Stomach of Young Dystrophic Children." Cand Med Sci, Tbilisi State Medical Inst, Tbilisi, 1953. (RZhBiol, No S, Dec 54)

Survey of Scientific and Technical Dissertations Defended at USSR Higher Educational Institutions (12)
SO: Sum. No. 556, 24 Jun 55

GNLOVANI, M.A., kand-med.nauk; SUJAVA, N.O.

Gase of renel diabetes combined with levulosuria. Pediatriia no.11:
85-86 N '57. (MIFA 11:2)

1. Iz kafedry gospital'noy pediatrii (zav. - prof. I.M.Rikhiladze)
Tbiliaskogo meditainskogo instituta (dir. - prof. I.T.Menteshashvili)
(DIABSTES)
(URINE-AHALYSIS AND PATHOLOGY)



GELOVANI, Meri Akvsentiyevna; KVACHADZE, Iosif Mikharoblovich

[Some characteristics of gastric secretion in dystrophic young children], [Nekotorye osobennosti zheludochmoi sekretsii u distradichnykh detei rannego vozrasta. Tbilisi, Gos.izd-vo "Sabchota Sakartvelo."] 1963. 178 p.[In Gaorgian]

(MIRA 17:4)

- 1. KAFYAN, A. G., GELOVANI, YE. S.
- 2. USSR (600)
- 4. Mulberry
- 7. Ways for accelerated growing of the mulberry tree.
 Dest. sel'khez. No.3, 1952

9. Monthly List of Russian Accessions, Library of Congress, January 1953, Unclassified.

: 63316 Tariford : Guitivated Plants. Industrial. Olefferous. CATEGORY Sugar. ABS. JOUR. : EZhBiol., No. 3, 1959, No. 11068 : Gelovani, Ye. 3. : Georgian Scientific desearch Institute of Sericulture. AUTHOR INST. : Nathods of Pro-Planting Grafting of Mu Derry. TITLE ORIG. PUB. : Byul. nauchno-tekhn. inform. Gruz. n.-i. in-ta shelkovodstva, 1957, Ho. 2, 9-26. : Methods of pre-planting grafts of mulberry (by the preplanting winter inoculation on the seedlings and by the ABSTRACT graft of a scion on rootstocks) suggested by Gorgian Scientific Research Institute of Sericulture (1948-1955) are described. In the winter inoculation, there were selected seedlings of the first grade which had stems of 8-10 rm diameter at the collum, the scedlings then being placed in a vessel with water (the temperature of the room was 15-200). Inoculation was performed with the eyes of the variety Gruziya by the usual method at the helight of 4-5 cm from the collum. The rooting in 1951 CAFD: 1/2

MICHALSKI, Eugeniusz; GELOWA, Helena

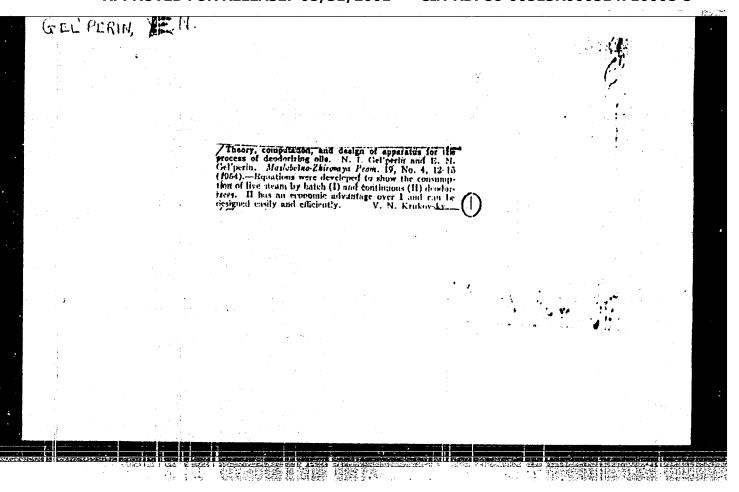
Catalytic determination of microgram amounts of germanium on the basis of amperometric measurements. Chem anal 8 no.4:643 163.

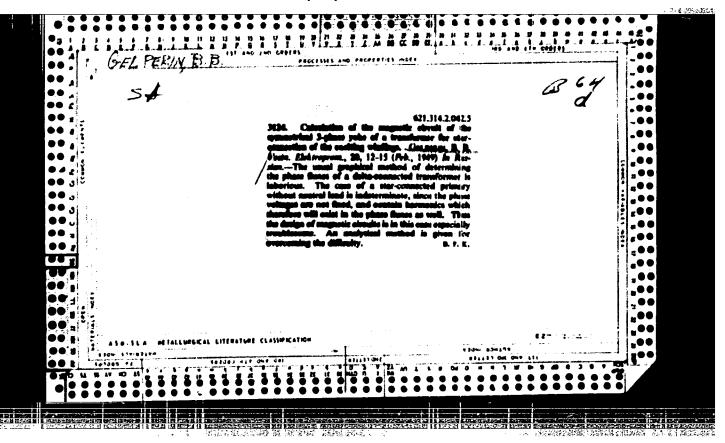
1. Department of Inorganic Chemistry, University, Lodz.

"Hoisting and conveying machinery" by A.A. Vainson [kand.tekhn.nauk].

Reviewed by A.I.Gal'perin. Mont.i spets.rzb.v stroi. 22 no.6:
31-32 Jl '60. (MIRA 13:7)

(Hoisting machinery) (Conveyers)





AUTHOR:

Gel'perin, B.B., Docent, Candidate of

Technical Sciences (Moscow)

105-58-5-11/28

工作 漢 经条件编制 机复数形式

TITLE:

Calculation Method of Saturation Chokes (Ketod rascheta

drosseley nasyshcheniya)

PERIODICAL:

Elektrichestvo, 1958, Nr 5, pp. 47-51 (USSR)

ABSTRACT:

A method for the calculation of chokes in the case of given technical characteristics with minimal dimensions, minimal weight, and involving low costs at permissible energy lesses is described. One of the possible constructions is investigated: The alternating current winding is fitted on to a core. Every winding can be divided into two parts and can be fitted to both cores, in which case they are connected in series or parallel. The optimal chokes haracteristics, viz. weight, dimensions and the operational characteristics, are influenced by the ratio between the weight

characteristics, viz. weight, dimensions and the operational characteristics, are influenced by the ratio between the weight of the active steel and the weight of the alternating current-winding ... M.... For the projecting of transformers M=2,5-3,5 is at present usual in the USSR. For saturation chokes his number applies to the ratio between the weight of the active steel and the total weight of D.C. — and A.C. windings. Basing on this

Card 1/2

Calculation Method of Saturation Chokes

105-58-5-11/28

number, it is possible to ascertain what magnitude of M is to be assumed in the here mentioned equations (11) - (15), in which case the weight of the copper of the D.C. winding must first be estimated. The magnetizing force for D.C. and A.C. is investigated separately and two equations (20), which are graphically represented, are derived. Further calculation of the chokes loss not differ from that of the transformer and is therefore not mentioned in this connection. There are 3 figures, and 4 references, 2 of which are Soviet.

SUBMITTED:

March 11, 1957

AVAILABLE:

Library of Congress

1. Saturable reactors--Mathematical analysis 2. Saturable reactors -- Design

Card 2/2

BURMAN, Petr Georgiyevich; KRAYE, Aleksandr Grigor yevich; GKL PERIN,
B.B., obshchiy red.; SKVORTSOV, P.P., obshchiy red.; TINOKHIMA,
V.I., red.; VORONIN, K.P., tekhn.red.

[Menufecture of magnetic circuits for transformers] Proisvodatvo magnitoprovodov transformatorov. Moskva, Gos.energ.izd-vo, 1959. 150 p. (Transformatory, no.3). (MIRA 13:2) (Electric transformers)

化对应作用于现代 医抗毒素

SHNITSER, L.M.; GEL'PERIN, B.B., red.; SKVORTSOV, P.F., red.; TIMOKHIMA, V.I., red.; ASANOV, P.M., tekhn.red.

[Principles of the theory and capacity of electric transformers]
Osnovy teorii i magruzochusia sposobnost' transformatorov. Izd.5,
perer. Moskva. Gos.energ.izd-vo. 1959. 230 p. (Transformatory.
no.1). (MIRA 13:7)

(Blectric transformers)

APPROVED FOR RELEASE: 08/31/2001 CIA-RDP86-00513R000514710008-5"

KAGANOVICH, Yevsey Aronovich; TIMOKHINA, V.I., red.; SKVORTSOV, P.P., insh., red.; GKL'PERIN, B.B., kand.tekhn.nauk, red.; ASANOV, P.M., tekhn.red.

[Testing of low and medium power transformers] Ispytanie transformatorov maloi i srednei moshchnosti. Moskva, Gos. energ.izd-vo, 1959. 239 p. (Transformatory, vyp.2).

(MIRA 13:3)

(Blectric transformers)

ALEKSENKO, Gennadiy Vamil'yevich; SKVORTSOV, P.P., red.; GEL'PERIN, B.B., red.; TIMOKHINA, V.I., red.; BORUNOV, N.I., tekhn.red.

[Parallel operation of transformers] Parallel naia rabota transformatory. Moskva, Gos.energ.izd-vo, 1960. 342 p. (Transformatory. no.5).

(Blectric transformers)

GEL'PERIH, B.B.; GUSAKOV, V.D.; LUBAN, Kh.L.; TROFIMOVA, H.N.

Tuning betatrons for maximum intensity. Prib.i tekh.eksp.
no.4:13-17 J1-Ag '60. (HIRA 13:8)

1. Moskovskiy transformatornyy zavod.
(Betatron)

87362

S/120/60/000/004/001/028 E032/E414

21,2300

AUTHORS:

Gel'perin, B.B., Gusakov, V.D., Luban, Kh.L. and

Trofimova, N.N.

TITLE: Methods of Adjustment of Betatrons to Maximum Intensity

PERIODICAL: Pribory i tekhnika eksperimenta, 1960, No.4, pp.13-17

The intensity of γ -rays produced by a betatron depends on a TEXT: large number of factors, all of which have to be taken into account in order to obtain the maximum possible intensity. present authors describe measures which were taken by them to ensure this maximum intensity. The first section of the paper describes devices which were used to obtain the optimum orbit radius. The radius of the orbit was controlled by special coils located on The emf induced in these coils by the electromagnet pole-face. the field produced by the electromagnet was balanced by externally applied emf. When the two emf's are in fact balanced, the radius of the orbit remains unaltered. If, on the other hand, the external emf is less than the emf induced in the coil, then the current produced in the coil gives rise to a magnetic flux which can be used to control the radius of the orbit. By plotting the intensity of the Y-rays as a function of the orbit radius, the Card 1/6

87352 5/120/60/000/004/001/028 E032/E414

Methods of Adjustment of Betatrons to Maximum Intensity

optimum radius can be determined. This scheme was used with a 15 MeV betatron in which the radius could be varied by 10 mm, using a current of 36 A. The second section of the paper is concerned with compensation of magnetic field nonuniformities in the air gap of the electromagnet. Since the static nonuniformity remains practically constant, only the phase nonuniformity of the field is considered. Of all the harmonics of the phase azimuthal field nonuniformity, only the first and the second are of importance in the betatron. Therefore, the compensation of the phase nonuniformity is reduced to the minimization of the first and The two harmonics are compensated by two groups second harmonics. of compensating coils which are located at 90° intervals. This is particularly simple in electromagnets with four-yoke construction as shown in Fig.4. It was found in the case of a 25 MeV betatron that the compensation of the phase nonuniformity increases the intensity by a factor of 2. The final section of this paper is concerned with devices which are capable of altering the field index n at the instant of injection. In the case of a 15 MeV Card 2/6

57362 5/120/60/000/004/001/028 E032/E414

Methods of Adjustment of Betatrons to Maximum Intensity

betatron two turns (in series) were used, having a radius equal to the radius of the equilibrium orbit. One of the turns was The turns were located above the chamber and the other below. connected through a stepdown transformer and a series resistor to the source supplying the electromagnet of the betatron. one turn was included in the circuit (sither the upper one or the lower one), no change in the intensity occurred when the current was varied between 0 and 0.7 A. However the intensity was increased by 20% when both coils were included, the current through them being 0.37 A. In one of the electromagnets it was found that there was a large phase shift along the radius and the shift increased with the radius. Although the static field index n for this magnet was 0.56 to 0.7 (in the region of the equilibrium orbit), the radial phase shift tended to increase n to about 1 at the instant of injection. This was counteracted by using distributed coils of the form shown in Fig.6. The coils were arranged so that the phase shift produced by them decreased with increasing radius. One group of such coils was placed below the

Card 3/6

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5/120/667600/004/001/028 E032/E414

Methods of Adjustment of Betatrons to Maximum Intensity

chamber and another above it, ensure that the field index n did not exceed a certain limiting value at the instant of injection. In some betatrons use was made above and below the chamber (Fig. 8). In a 15 MeV betatron, the These consisted of two turns located γ-ray intensity was increased by the superposition of an additional field at the instant of injection over a 130° sector. This was achieved with the aid of two four-turn coils, placed above and below the chamber respectively (Fig. 9). There are 9 figures and

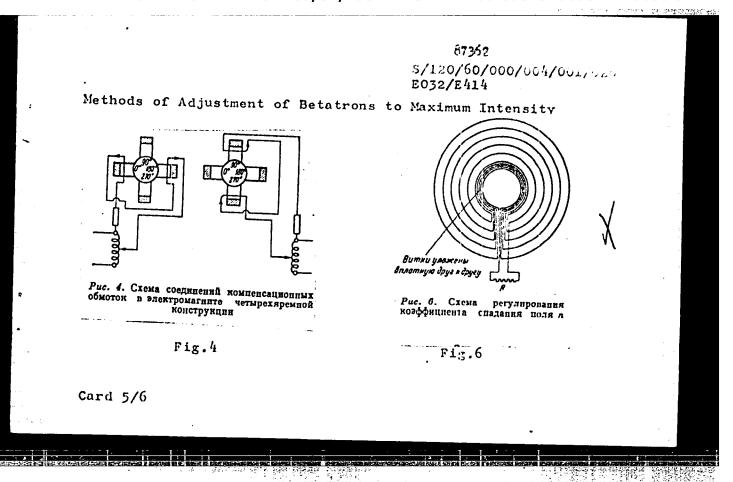
ASSOCIATION: Moskovskiy transformatornyy zavod

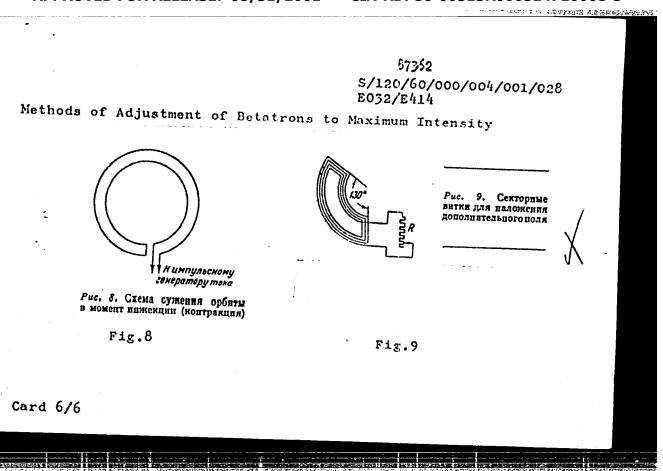
(Moscow Transformer Factory)

SUBMITTED:

July 10, 1958 (initially) June 9, 1959 (after revision)

Card 4/6





ANSHIN, Vladimir Shayevich; KRAYZ, Aleksandr Grigor'yevich; GEL'PERIN, B.B., red.; SKVORTSOV, P.P., red.; TIMOKHINA, V.I., red.; VCRONIN, K.P., tekhn.red.

> [Assembly of large transformers] Sborks mushchnykh transformatorov. Moskvs, Gos.energ.isd-vo, 1961. 463 p. (Transformatory, MIRA 14:4)

1. Moskovskiy elektrosavod imeni V.V.Kuybysheva (for Anshin, Krays).

(Electric transformers)

CIA-RDP86-00513R000514710008-5" APPROVED FOR RELEASE: 08/31/2001

CHERNICHKIN, D.S.; BORISENKO, N.I.; MESHCHERYAYKOV, K.N.; KOMAR, Ye.G.; PEDULOV, L.N.; KOZLINSKIY, V.A.; MAKSIMOV, A.S.; GEL'PERIK, B.B.

Professor D. V. Efremov; obituray. Elektrichestvo no.2:95-96 F 161. (MIRA 14:3) (Efremov, Bmitrii Vasil'evich, 1900-1961)

CIA-RDP86-00513R000514710008-5" APPROVED FOR RELEASE: 08/31/2001

5/196/61/000/010/017/037 E194/E155

AUTHOR:

Geliperin, B.B.

TITLE:

Calculation of the magnetic leakage field of a coil

with steel core and air gap

PERIODICAL: Referativnyy zhurnal, Elektrotekhnika i energetika, no.10, 1961, 12, abstract 101 82. (Vestn. elektroprom-

sti, no.3, 1961, 21-25)

A method is proposed which gives simple equations for calculating the magnetic field of a coil near a gap in the steel core, allowing for the location of the magnetising coil and also for the final permeability of the steel. Calculations show that the magnetic leakage field of the coil may be represented by the magnetic field of a current in an infinitely thin lamina. If it is necessary to allow for the influence of the magnetising winding then a magnetising winding of natural dimensions and arrangement is introduced into the equivalent circuit; allowance must also be made for reflection of the winding from the steel surface. An example is given of an equivalent circuit which

Card 1/2

Calculation of the magnetic ... \$/196/61/000/010/017/037

allows for the magnetising winding. The calculation procedure is given. A calculation is also given of the influence of core saturation of the magnetic leakage flux in the magnet poles. 5 illustrations.

[Abstractur's note: Complete translation.]

Card 2/2

ALEKSENKO, Gennadiy Vesil'ye daha A. Male 10th, Ashryatov Ali; SOLOMONOVICH, Frid Yefim; GEL'HERIN, B.B., red.; SKVORTSOV, P.P., red.; KRAYZ, A.I., Ped.; BORUNOV, N.I., tekhn. red.

> [Testing of high-voltage power transformers and autotransformers] Ispytaniia vysokovol'tnykh i moshchnykh transformatorov i avtotransformatorov. Moskva, Gosenergoizdat. Pt.l. 1962. 671 p. (Transformatory, no.8) (MIRA 16:10)

(Electric transformers--Testing)

GEL'PERIN, B.B., kand.tekhn.nauk; ZLOBINSKIY, E.L., inzh.

Mathod for calculating a stabilizer based on the principle of a regulated choke. Vest. elektroprom. 34 no.4:32-38 Ap 163.

(MIRA 16:10)

OEL'PERIN, N.1., professor, doktor tekhnicheskikh nauk; GEL'PERIN, E.N., inzhener-tekhnolog.

Rectification of binary mixtures consisting of components having mutual partial solubility. Gidroliz.i lesokhim.prom. 10 no.4:3-6 (Distillation) (Distillation)

GEL'PERIN, N.I.; AYNSHTEYN, V.G.; GEL'PERIN, E.N.; L'VOVA, S.D.

Hydrodynamic characteristics of the fluidization of granular materials in conical-cylindrical units. Thim i tekh topl i masel 5 no.8:51-57 Ag '60. (MIRA' 3:8)

1. Moskovskiy institut tonkoy khimicheskoy tekhnologii im. M.V. Lomonosova.

(Fluidization) (Granular materials)

Determination of the coefficient of heat transfer in conical reactors having a granular solid fluidized bed. Zhur.VKHO 6 no.3:349-350 '61. (MIRA 14:6) (Fluidization) (Heat—Transmission)

APPROVED FOR RELEASE: 08/31/2001 CIA-RDP86-00513R000514710008-5"

GEL'ERIN, E.N.; FRAYMAN, R.S.

Studying the heat transfer from conical surfaces to a fluidized bed.
Khim.prom. no.11:806-816 '63. (MIRA 17:4)

FRAYMNA, R.S.; GEL'PERIN, E.N.; BOBNEVA, A.A.

Multizonal apparatus for carrying out processes in a fluidized bed. Khim.prom. no.11:827-830 N '62. (MIRA 16:2)

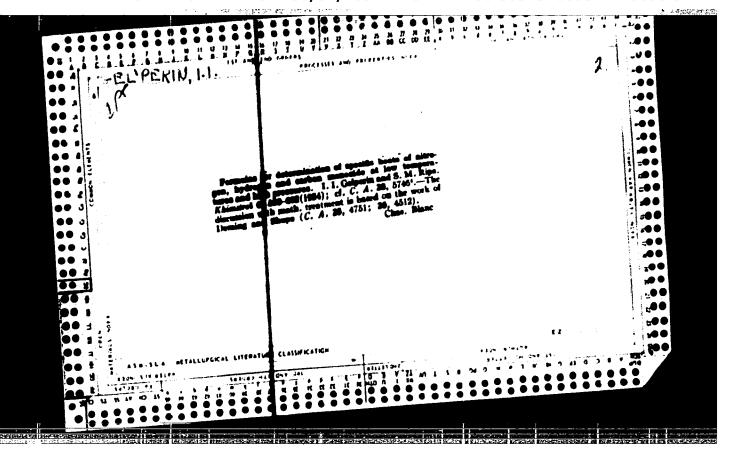
(Fluidization—Equipment and supplies)

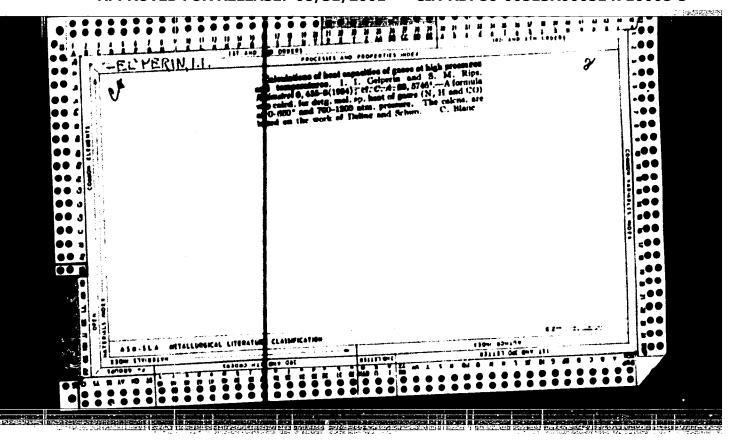
FRAYMAN, R.S.; GEL'PERIN, E.N.; LUZANOVA, T.I.

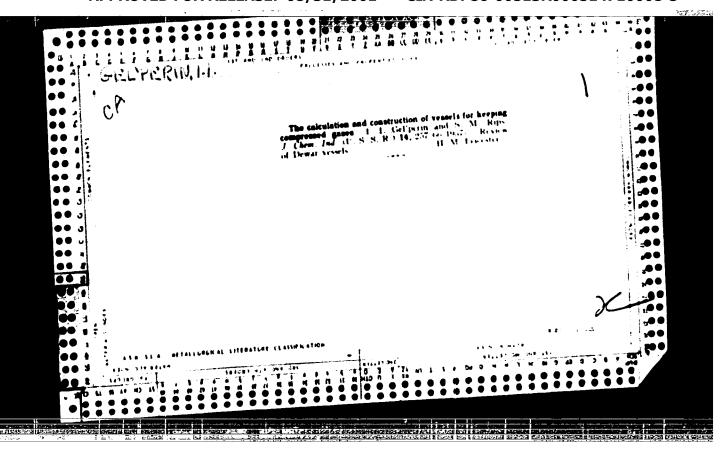
Gas-distributing units with conjugate cones for the apparatus with a fluid bed. Khim.i tekh.topl.i masel 8 no.8:44-46 Ag '63.

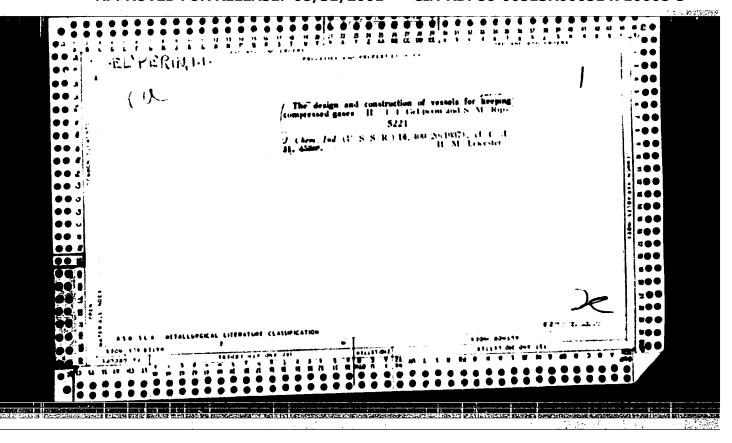
(MIRA 16:9)

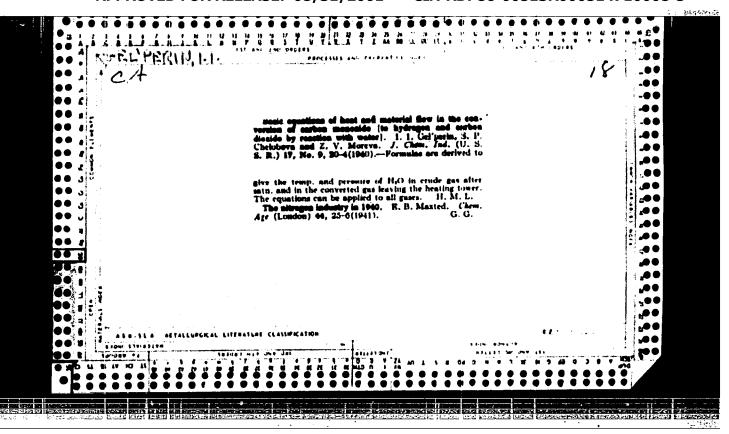
(Gas distribution) (Fluidization)

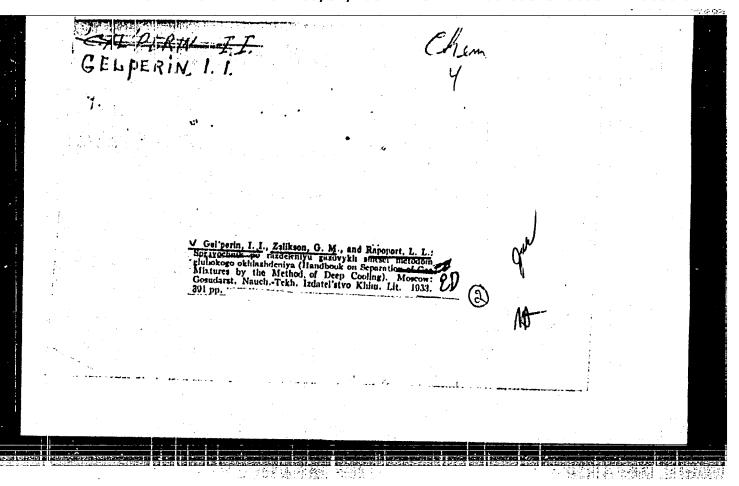












Translation from: Referativnyy zhurnal, Mekhanika, 1958, Nr 2, p 67 (USSR)

AUTHORS: Gel'perin, I. I., Rapoport, L. L.

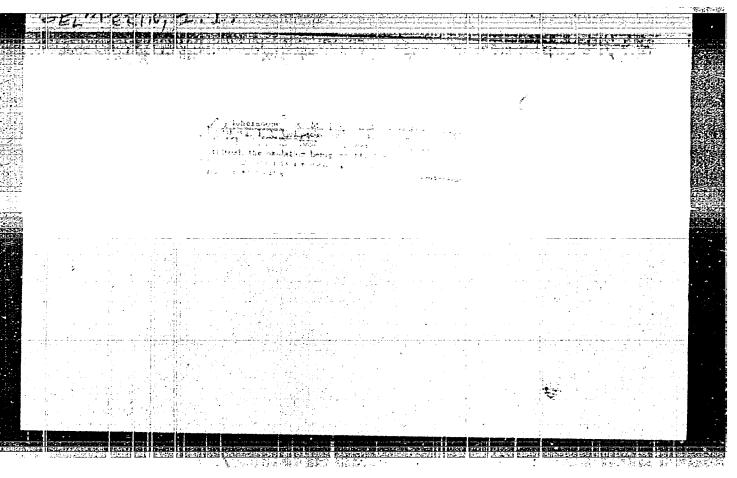
TITLE: The Hydraulic Resistance of Coiled Heat Exchangers (Gidravlicheskoye soprotivleniye vitykh teploobmennikov)

PERIODICAL: Tr. Gos. n. -i. i proyektn. in-ta azotn. prom-sti, 1954, Nr 3, pp 193-199

ABSTRACT: It is shown that the calculation of the hydraulic resistance of a coiled heat exchanger according to formulas obtained from tests made on a bundle of tubes of relatively low solidity ratio yields an overrated value for the hydraulic resistance. An empirical formula is obtained for the calculation of the hydraulic resistance of the high-solidity bundle of tubes comprising a coiled heat exchanger.

I.S. Simonov

Card 1/1



Using heat-elimination surfaces for controlling temperature in the zone of catalysis. Khim. nauka i prom. 2 no.2:233-237 '57.

(Catalysis)

(Heat--Transmission)

(MIRA 10:6)

Special characteristics of the calculation for the removal of carbon monoxide with liquid nitrogen. Trudy GIAP no.8:213-218

(Carbon monoxide) (Mitrogen) (Gas--Furification)

Jefferking Lad

57-9-29/40

AUTHOR:

Gel'perin, I.I., Minsker, K.S.

TUTLE:

Determination of the Heat Exchange Surface if the Final Difference of Temperature Between the Heat Carrier and One of the

Cooling Agents is Equal to Zero.

(Opredeleniye poverkhnosti teploobmena v sluchaye, kogda konechnaya raznost'temperatur teplonositelya i odnogo iz khadoagentov

ravna nulyu)

PERIODICAL:

Zhurnal Tekhn. Fiz., 1957, Vol. 27, Nr 9, pp. 2143 - 2148 (USSR)

ABSTRACT:

The method described here makes it possible to determine the necessary heat exchange surface without having to ascertain the average logarithmic temperature drop. Countercurrent- and direct current heat exchange processes are investigated for the case that the final temperature drop between the heat carrier and one of the cooling agents is equal to zero. Equations are derived with the aid of which it is possible to determine the necessary length of heat exchange tubes without having to use the basic equation of heat exchange Q = kF \(\Delta \) t, which is not applicable to the present case. The equations derived here make it possible to determine the intermediary temperatures and the amount of emitted heat corresponding to these temperatures at every

Card 1/2

57-9-29/40

Natermination of the Heat Exchange Surface if the Final Difference of Temperat-

ures Between the Heat Carrier and One of the Cooling Agents is

Equal to Zero

part of the system with equal ease. A complete example is com-

puted. There are 4 figures and 2 Slavic references.

SUBMITTED: February 20, 1957

AVAILABLE: Library of Congress

Card 2/2

DUACE T DOOY EYDIOTMATTON

SELTERIE II.

PHASE I BOOK EXPLOITATION SOW 5604

- Atroshchenko, Vasiliy Ivanovich, Iosif Il'ich Gel'perin, Anatoliy Petrovich Zasorin, Viktor Ivanovich Konvisar, Antonina Yakovlevna Kraynyaya, Agnessa Grigor'yevna Leybush, and Anism Rudol'fovich Yastrebenetskiy
- Metody raschetov po tekhnologii svyazannogo azota (Computational Methods in the Technology of Combined Nitrogen) Khar'kov, Izd-vo Khar'kovskogo univ., 1960. 302 p. 5,000 copies printed.
- Ed. (Title page): V.I. Atroshchenko; Ed.: D.A.Vaynberg; Tech. Ed.: V.S. Zadorozhnyy.
- PURPOSE: This textbook is intended for graduate students in chemical technology institutes, and may also be used by engineering and technical personnel of the chemical industry.
- COVERAGE: The book describes computational methods used in the industrial production of hydrogen, nitrogen, synthetic ammonia, urea, nitric acid, and methanol. Problems in the refining of natural gas are also reviewed. The computations involve material and heat balances and the determination of

Card-1/5

Computational Methods (Cont.)

SOV/5604

dimensions of equipment and its design, based on equations of chemical reactions and thermodynamic computations of possible yields or reaction rates per se. Equations and formulas for determining reaction rates are also given. Plant outputs, flow sheets, and technical characteristics are included. The supplement includes an equilibrium state (vapor phase) diagram of a nitrogen-oxygen system; entropy diagrams for ammonia, air, nitrogen, and oxygen; graphs of heat capacity, viscosity, and heat conductance vs. temperature (0-350°C) for nitrogen-hydrogen-ammonia mixtures at P = 300 atm; a viscosity vs. percentage composition graph of CO + H2 mixture at 50 - 400° C; diagrams of CH4, CO2, CO, N2, and H2 solubility in CH3OH at 300 atm and 25° C; a compressibility coefficient vs. temperature (25 - 250° C) graph of CO + 2 H_2 mixtures at 250 and 300 atm; a nomogram of physical constants; enthalpy vs. temperature diagrams for alcohols, olefins and methanol; and tables of rate constants, partial pressures, heat contents of solutions, viscosities of gases, average molecular heat capacities of various gases and vapors at different pressures, rate constants of the oxidation of nitric oxide by oxygen at different temperatures, etc. The authors are affiliated with the Khar kovskiy politekhnicheskiy institut imeni V.I. Lenina (Khar kov Polytechnic Institut imeni V.I. Lenin) and the Gosudarstvennyy institut azotnoy

Card-2/5

Computational Methods (Cont.) SOV/5604 promyshlennosti i produktov organicheskogo sinteza (State Institute for the Mitrogen Industry and Products of Organic Synthesis). The Introduction and Chs. V, X, and XI were written by V.I. Atroshchenko; Ch. I, by A.G. Leybush; Chs. II, III, VI, and VII, by A.R. Yastrebenetskiy; Ch. IV, by I.I. Gel'perin; Chs. VIII and XIV, by V.1. Konvisar; Chs. IX and XIII, by A.P. Zasorin; and Ch. XII, by A. Ya. Kraynyaya. No personalities are mentioned. References, mainly Soviet, accompany individual chapters. TABLE OF CONTENTS: Foreword 3 Introduction 4 Ch. I. Computations and Design of a Methane Conversion Plant 5 Ch. II. Computations and Design of a Carbon Dioxide Conversion Plant 37

Card 3/5

GEL PERIN, I.I., kand tekhn.nauk; DARYUSIN, A.D., kand tekhn.nauk

Prevention of explosions in apparatus for the separation of coke gas by the method of deep cooling. Zhur. VKHO
7 no.6:661-666 '62.

(Coke-oven gas)

(Combustion, Spontaneous)

MINNES IN

S/064/63/000/002/004/005 B117/B186

AUTHORS:

Gel'perin, I. I., Kagan, A. M.

TITLE:

Effect of thermal conductivity of granular substances on the heat exchange of the gases passing through these substances

PERIODICAL: Khimicheskaya promyshlennosti, no. 2, 1963, 52 - 55

And the fact of the party of th

TEXT: The heat transfer of granular substances was studied on the gases passing through them in a U-shaped tube, of 12 mm diameter, heated with boiling water. 8 Fractions of granular substances having different thermal conductivities were used. Packings of these substances were filled into the tube in a section 408 mm long. The mass flow rate of the air was varied from 0.6 to 7.3 kg/cm²-sec during the experiments. The air temperature at the inlet and the outlet of the tube was measured by copperconstantan thermocouples with a special device for averaging the temperature of the air current. The temperature of the tube walls was measured with five thermocouples fitted into them. The mean temperature difference between gas and tube wall was determined by a planimeter from the area bounded by the temperature curves. The accuracy of the experiments was guaranteed by the fact that the heat transfer coefficient was not influenced Card 1/2

Effect of thermal conductivity ...

\$/06.1/63/000/002/004/005 B117/B186

by other variable factors (achieved through same size and shape of grains). The heat transfer coefficient was not found to be influenced considerably by the thermal conductivity of the material. This is explained by the thermal resistance of the boundary layer on the tube wall being higher than the resistance of heat transfer from the core to the wall. When the granular layer of the material is heated without gas current it was found that only the length of the period until stationary conditions set in is influenced by the thermal conductivity and the thermal capacity of the granular material. There are 4 figures and 3 tables.

Card 2/2

GEL'PERIN, I.I.; KACAN, A.M.

Effect of the heat conductivity of granular materials on the heat transfer in gases passing through them. Khim. prom. no.2:132-135 F *63. (MIRA 16:7)

(Granular materials—Thermal properties)
(Gases) (Heat—Transmission)

KAGAN, A.M.; GEL'PERIN, I.I.

Effect of the thermophysical properties of gases on their heat transfer in the presence of granular materials. Khim. prom. no.8:620-622 Ag '63. (MIRA 16:12)

三世紀 法国际工程的 医二种

GEL'PERIN, I.I.; KAGAN, A.M.

Direction of the heat flow and its effect on the heat transfer of gases in packed tubes. Khim,prom. no.11:859-865 '63.

(MIRA 17:4)

KAGAN, A.M.; ŒL'PĒRIN, İ.I.

Stabilization of the process of heat transfer in packed tubes. Zhur. VKHO 9 no. 2:233-234 *64. (MIRA 17:9)

1. Gosudarstvennyy institut azotnoy promyshlennosti.

GEL*PERIN, 1.1.; KALININA, S.Ye.; RAPOPŒT, L.L.

Production of heavy water from a nitrogen-hydrogen mixture.
Khim. prom. no.6:475-479 Je *64.

(MIRA 18:7)

L 18381-65 EWG(j)/EWF(m)/EPF(c)/EPR/EWP(t)/EWP(b) Pr-4/Ps-4/Pb-4 IJP(c) JD
ACCESSION NR: APS003110 S/0063/64/009/003/0289/0299

AUTHOR: Golfreria, I. I. (Cardidate of technical sciences); Daryusin, A. P. (Cardidate of technical sciences)

TITLE: Contamination of hydrocribon conversion gases by nitrogen oxides and their danger of scrubbing carbon monoxide with liquid nitrogen

SOURCE: Vsesoyuznoye khimicheskoye obshchestvo. Zhurnal, 7. 9, no. 3, 1964, 289-299

TOPIC T/GS: carton monoxide, liquid nitrogen, nitrogen oxide, hydrocarbon, chemical reaction

Abstract: Scrubbing carbon monoxide with liquid nitrogen permits the production of a nitrogen-hydrogen mixture of high purity, not containing appreciable amounts of catalytic poisons and contaminants for ammonia synthesis. However, in 1961, reports were published of explosions of low-temperature blocks in which converted gas was acrubbed with nitrogen in Holland, Japan, and the US. Which converted gas was acrubbed with nitrogen in Holland, Japan, and the US. The main reason for these explosions was believed to be complexes which were formed as the result of the low temperature interaction of nitrogen oxides with reactive organic micro-impirities present in the converted gas and accumulating in the low-temperature block apparatus. It must be noted that despite limited information on the exact reactions involved, several

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L 18381-65 ACCESSION NH: APSC03110 restrictions are ustablished experimentally and greater operating safety can be achieved by: a) having a minimum of accumulated nitrogen oxides in the low-temperature block after the run, as calculated from the amount of nitrogen oxide entering the block from the separated gases; b) maintaining a maximum permissible nitrogen oxide content in the gas to be separated; c) strictly regulation of brief, extended and total shutdown of the low-temperature block after heating and scrubbing. Orig. art. has 1 figure, 11 graphs, 10 tables.
ASSOCIATION: none SUBMITTED: ENCL: SUB CODE: FP. GC NO REF SOV: 003 OTHER: **JPRS** Card 2/2

GEL'PERIN, I.I.; KAGAN, A.M.

Heat emission from boiling water at small thermal leads. Khim.prom. 40 no.8:616-619 Ag '64. (MIRA 18:4)

1、特別的問題。 電影 在 數十一

人名伊里斯 医巴拉斯氏 187 基金铁矿

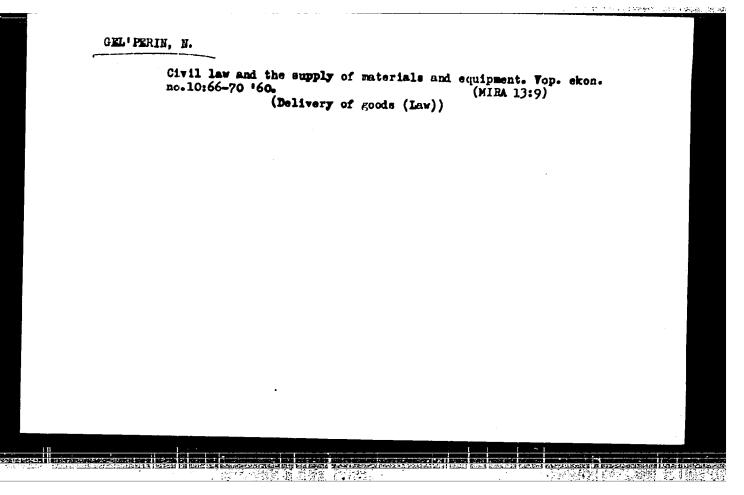
ZAREMBO, G.V., inzh.; GEL'PERIN, L.A., inzh.

Redesigned MP-21 press. Masl.-zhir. prom. 28 no.10:29-31 0 '62. (MIRA 16:12)

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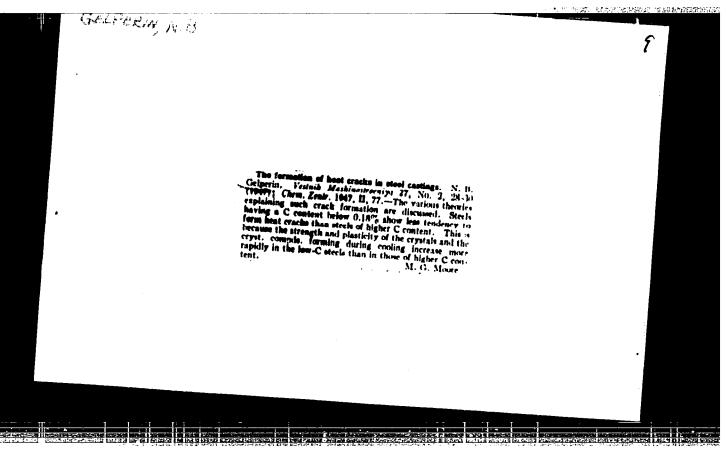
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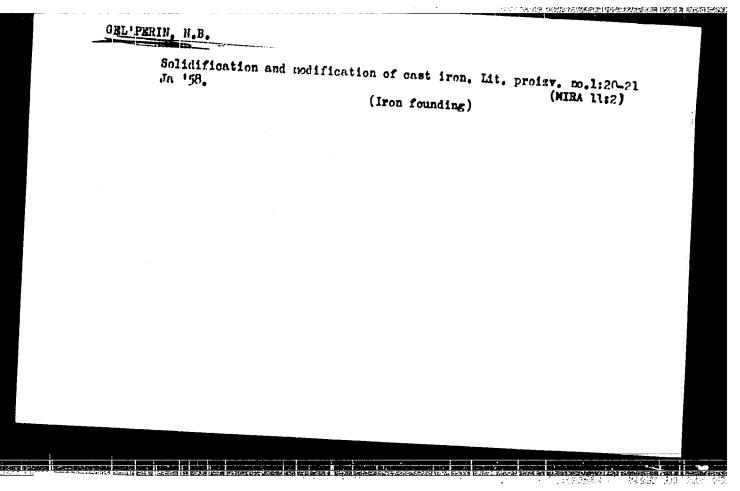


LIVSHITS, Mikhail Naftol'yevich; BALABANOV, Ye.M., doktor fiziko-matematicheskikh nauk, nauchnyy redaktor; GEL'PERIM, H.B., kandidat tekhnicheskikh nauk, nauchnyy redaktor; GEMPEL'SON, A.Z., redaktor; GLADEIEH, N.N., tekhnicheskiy redaktor

[Electric methods of painting, enameling and glazing] Blektricheskie metody okraski, emalirovaniis i glasurovaniis izdelii. Moskva, Gos. izd-vo lit-ry po stroit. materialam. 1956. lll p. (MLRA 10:3) (Spray painting) (Especial and enameling) (Glazing)

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18(5), 25(5)

AUTHOR: Gel'perin, N.B., Candidate of Technical ociences SOV/128-59-4-9/27

TITLE: Improved Technology in Producing Cast Crankshafts

PERIODICAL: Liteynoye Proizvodetvo, 1959, Nr 4, pp 16-19 (USER)

ABSTRACT:

By replacing the forged crankchafts of combustion motors by cast crankshafts, a considerable amount of metal and labor is saved. The crankshafts are cast of carbonized, graphitic, and alloyed steel, of alloyed grey iron, of cast iron containing magnesium, or even of malleable cast iron. It is very important to select the materials to be used for crankshafts which are exposed to great strain as in tractor and combine motors. Plasticity and toughness of the material in this case are of secondary importance. It is essential to know the point at which the material starts tiring. Cast iron containing magnesium proved to be the perfect material. Its surface hardness assures the required wear resistance of the trun-

Producing cartings from magnesium cast iron, Card 1/2 the technology in regard to atructure and qualities

Improved Technology in Producing Cast Crankshafts

was not certain. A parallel production of crankshafts from malleable cast iron was therefore necessary. At the present time, the production of crankshafts from magnesium cast iron is being organized in the "Serp i molot" (Hammer and bickle) works. Provisions for production from malleable cast iron have also been made. The original construction of the crankshafts was totally non-technological. It was improved later on, but not all defects could be removed. A technologically better design resembling the crankshaft in form and dimensions was created for the D motor DW-30 (Figure 1). The following part of the article discusses molds, molding compounds, production and composition of the magnesium cast iron, removal of inclusions, and the melting aggregate consisting of a cupola with blast heater and heated forehearth. There

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